7234

April 27, 1960

ENVIRONMENTAL LEVELS OF RADIOACTIVITY

Report for 1959

Data Compiled by:

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Introduction

Radioactive waste materials arising from the operation of atomic energy installations at Oak Ridge are collected, treated, and disposed of according to their physical states.

Solid wastes are buried in a Conasauga shale formation. This shale has a marked ability to fix radioactive materials by an ion exchange mechanism.

Liquid wastes which contain long-lived fission products are confined in storage tanks or are released to earthen pits located in the Conasauga shale formation. Low level liquid wastes are discharged, after preliminary treatment, to the surface streams.

Air that may become contaminated by radioactive materials is exhausted to the atmosphere from several tall stacks after treatment by means of filters, scrubbers, and/or precipitators.

Due to the nature of operations at the three Oak Ridge installations (ORNL, ORGDP, Y-12), there is some variation in methods of monitoring and reporting of results. Therefore, monitoring methods as they are employed at each of the three installations will be discussed.

OAK RIDGE NATIONAL LABORATORY (X-10)

Air Monitoring

Atmospheric contamination and fall-out occurring in the general environment of East Tennessee are monitored by two systems of monitoring stations. One system consists of seven stations which encircle the plant areas (Fig. 1) and provides data for evaluating the impact of all Oak Ridge operations on the immediate environment. A second system consists of eight stations encircling the Oak Ridge area at distances of from 12 to 120 miles (Fig. 2). This system provides data to aid in evaluating local conditions and to assist in determining the spread or dispersal of contamination should a major incident occur.

Three types of samples are collected at the stations. One type is taken by passing air continuously through filter paper. The filter paper will collect only those particulates considered to be respirable. A second type utilizes a gummed paper technique for collecting fall-out. The fall-out trays collect the heavier particles as well as the respirable particles. A third type is rain water which provides data for determining the soluble and insoluble fractions of the radioactive contamination.

Data obtained from the various sampling methods are accumulated and tabulated. In the case of the filter samples, data are tabulated in average $\mu c/cc$ of air sampled and numbers of particles per 1000 ft of air sampled. In the case of gummed paper fall-out collection, data are tabulated in $\mu c/ft^2$ and numbers of particles per ft . In the case of rain water, data are tabulated in average $\mu c/cc$ of rainfall collected. The data are compared to established maximum permissible concentrations and with previous averages.

Water Monitoring

Large volume, low level liquid wastes originating at Oak Ridge National Laboratory are discharged, after some preliminary treatment, into the Tennessee River system by way of White Oak Creek and the Clinch River. Releases are controlled so that resulting average concentrations in the Clinch River comply with the maximum permissible levels for population in the neighborhood of a controlled area as recommended by the National Committee on Radiation Protection (NCRP). The concentration of radioactivity leaving White Oak Creek is measured and concentration values for the Clinch River are calculated on the basis of the dilution provided by the river.

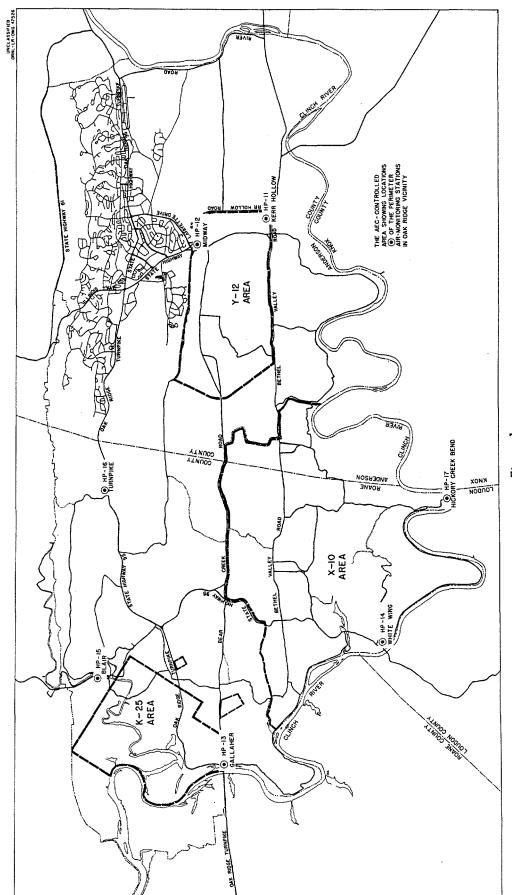
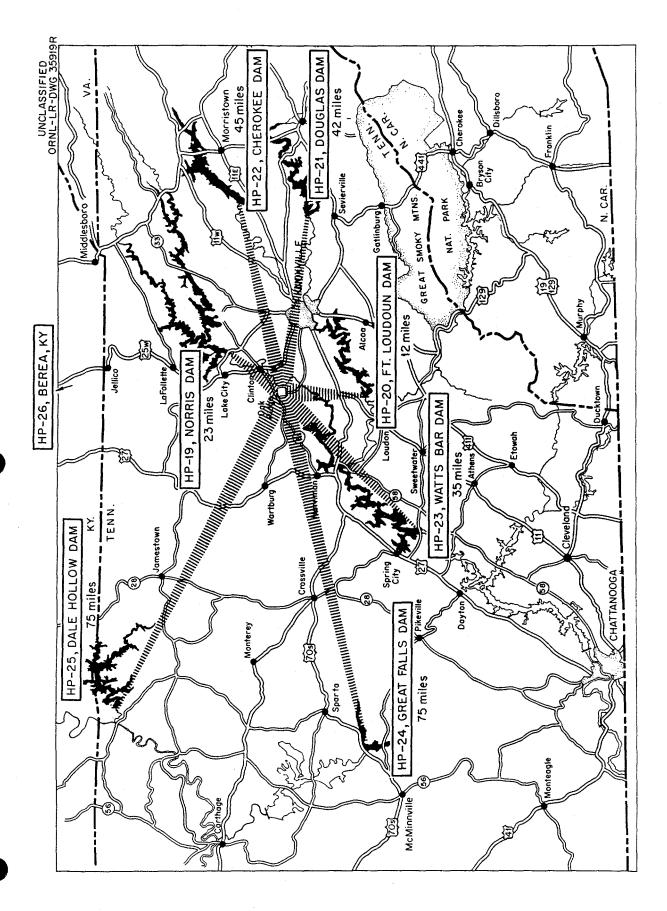


Figure 1



STATION SITES FOR REMOTE AIR MONITORING SYSTEM

Radioactive liquid wastes leaving the Laboratory are sampled at a number of locations as shown in Fig. 3. Daily samples are taken where the effluent leaves the Laboratory, at a point where wastes enter the public waterway, and at Centers Ferry near Kingston, Tennessee, the first population center downstream from the A.E.C. controlled areas. In order to establish background conditions, daily samples are collected also in the Clinch River 17 miles upstream from the point of entry of the waste. Stream gauging operations are carried on continuously by the United States Geological Survey to obtain dilution factors for calculating the concentrations of wastes in the river.

The fraction of the total beta activity comprised by each isotope is determined from analysis of long-lived radionuclides contained in the effluent and a weighted average maximum permissible concentration for water, $(MPC)_W$, for the mixture of radionuclides is calculated on the basis of the isotopic distribution using the MPC values of each isotope as recommended by the NCRP. The average concentrations of radioactivity in the Clinch River are compared to the calculated $(MPC)_W$ value.

Annual surveys of the Clinch and Tennessee Rivers are conducted to determine the extent of dispersion of radioactive material in river sediment. This survey is required in order to determine whether or not there is a significant build-up of radioactive constituents in the river system. Gamma radiation measurements are made on the bottom sediments. Sediment samples are radiochemically analyzed for long-lived radioactive isotopes.

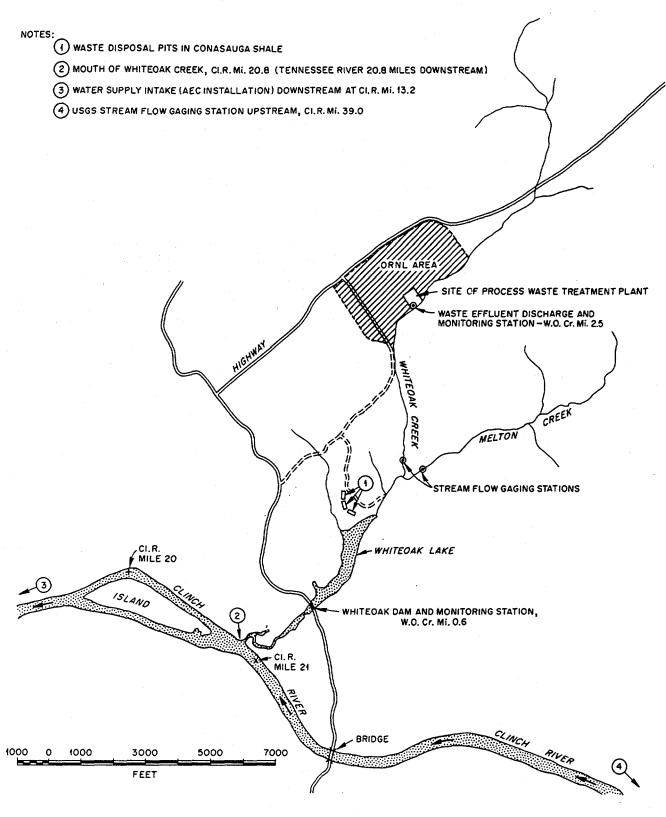
Gamma Measurements

External gamma radiation levels are measured monthly at five locations in the Oak Ridge area. Measurements are taken with a Geiger-Muller tube at a distance of three feet above ground and the results are tabulated in terms of mr/hr.

Discussion of Data

Data accrued from the monitoring system in 1959 are presented in Tables I through VIII.

The air contamination levels shown by the continuous air monitoring systems for the immediate and remote environs of the Oak Ridge area were 1.6% and 1.4% respectively of the maximum permissible concentration for populations in the neighborhood of a controlled area. Air contamination levels during the first half of 1959 were a factor of 4 to 6 times greater than the average for the entire year. By the end of 1959 air contamination levels had decreased to approximately 1/5 the value given for the yearly



Location Sketch Map ORNL Area Surface Drainage

Figure 3

average. Specific analysis for fission products and decay studies indicated that the high levels experienced during the first part of the year were due to the type of fall-out from world-wide weapons testing. The low values for remote stations 23 and 24 resulted from the fact that these stations were in operation only during the latter half of 1959 and do not reflect the higher fall-out levels experienced during the first half of the year.

Fall-out data and rain water data followed the same trend shown by the continuous air monitoring data.

The probable average concentrations of radioactivity in the Clinch River at Mile 20.8, the point of entry of the wastes, and at Mile 4.5, near Kingston, Tennessee, were 3.1 x 10-7 μ c/cc and 4.9 x 10-8 μ c/cc respectively. These values are 25.4% and 22.3% of the weighted average maximum permissible concentration for populations in the neighborhood of a controlled area as recommended by the NCRP. The average concentration of transuranic alpha emitters in the Clinch River at Mile 20.8 was 3 x 10-10 μ c/cc, which is 0.03% of the weighted average (MPC) $_{\rm W}$ value.

The concentration of radioactivity in the sediment of the Clinch River drops off materially after the first 20 miles downstream from the entry of White Oak Creek and approaches background levels 200 miles downstream. The average radiation level for the cross section where the highest levels were encountered was approximately 19 times the measured background levels or 0.12 mr/hr. This point is located 4.5 miles below the outfall of White Oak Creek. At 100 miles downstream the average level was approximately twice background.

External gamma radiation levels in the Oak Ridge area averaged 0.024 mr/hr. This level does not differ significantly from the average of the levels measured throughout the United States by the U. S. Public Health Service Radiation Surveillance Network.

TABLE I CONTINUOUS AIR MONITORING FILTER DATA Units of 10-13 $\mu c/cc$

| Station Number | Location | Number of Samples Taken | Maximum | Minimum | Average | % of (MPC)* |
|--|---|--|---|--|--|---|
| | | Perimeter | Stations | | | |
| HP-11 HP-12 HP-13 HP-14 HP-15 HP-16 HP-17 Average | Kerr Hollow Gate Midway Gate Gallaher Gate White Wing Gate Blair Gate Turnpike Gate Hickory Creek Bend | 52 49 52 52 52 52 52 | 47.52 81.31 58.52 42.48 61.06 51.61 60.27 | 0.49 0.08 0.54 0.49 0.45 0.28 0.17 | 15.77 16.29 16.63 11.30 19.97 13.48 16.86 | 1.6 1.7 1.1 2.0 1.4 1.7 |
| | | Remote St | tations | | | |
| HP-19 HP-20 HP-21 HP-22 HP-23** HP-24** HP-25 HP-26 | Norris Dam Loudoun Dam Douglas Dam Cherokee Dam Watts Bar Dam Great Falls Dam Dale Hollow Dam Berea, Kentucky | 52 52 37 39 29 26 46 52 | 86.20 90.49 58.17 100.52 35.14 10.58 78.91 54.27 | 0.57 0.65 0.68 0.52 0.49 0.24 0.76 | 23.23 22.11 10.91 16.01 5.13 2.53 18.04 13.77 | 2.3 2.2 1.1 1.6 0.5 0.3 1.8 |
| Average | | | | | 13.97 | 1.4 |
| | | | | | | |

^{* (}MPC) is taken to be 10-10 $\mu c/cc$ as recommended in NBS Handbook 69, Table 4, p. 94. ** Stations in operation only during latter half of 1959.

TABLE II

CONTINUOUS AIR MONITORING FILTER DATA

Particles/1000 cu. ft. of Air Sampled

| Station Number | Location | Number of Samples Taken | Maximum | Minimum | Average |
|-------------------|--------------------|----------------------------|---------|---------|---------|
| | | Perimeter Sta | ıtions | | |
| HP-11 | Kerr Hollow Gate | 52 | 6.27 | 0.00 | 1.20 |
| HP-12 | Midway Gate | 49 | 6.81 | 0.00 | 1.29 |
| HP-13 | Gallaher Gate | 52 | 5.08 | 0.00 | 0.95 |
| HP-14 | White Wing Gate | 52 | 5.91 | 0.00 | 0.82 |
| HP-15 | Blair Gate | 52 | 10.29 | 0.00 | 1.52 |
| HP-16 | Turnpike Gate | 52 | 5.39 | 0.00 | 0.86 |
| HP-17 | Hickory Creek Bend | 52 | 7.22 | 0.00 | 1.02 |
| Average | | | | | 1.09 |
| | | Remote Stati | lons | | |
| HP-19 | Norris Dam | 52 | 7.98 | 0.00 | 1.64 |
| HP-20 | Loudoun Dam | 52 | 6.61 | 0.00 | 1.43 |
| HP-21 | Douglas Dam | 37 | 2.83 | 0.00 | 0.28 |
| HP-22 | Cherokee Dam | 39 | 7.26 | 0.00 | 0.54 |
| HP-23* | Watts Bar Dam | 29 | 0.40 | 0.00 | 0.05 |
| HP-24* | Great Falls Dam | 26 | 0.14 | 0.00 | 0.02 |
| HP-25 | Dale Hollow Dam | 46 | 7.96 | 0.00 | 1.01 |
| HP-26 | Berea, Kentucky | 52 | 5.83 | 0.00 | 1.10 |
| Average | | | | | 0.76 |

TABLE III

GUMMED PAPER FALL-OUT DATA

Units of 10^{-l4} µc/sq. ft.

| Station Number | Location | Number of Samples Taken | Maximum | Minimum | Average |
|---|---|--|--|--|--|
| | | Perimeter Sta | ations | | |
| HP-11 HP-12 HP-13 HP-14 HP-15 HP-16 HP-17 | Kerr Hollow Gate Midway Gate Gallaher Gate White Wing Gate Blair Gate Turnpike Gate Hickory Creek Bend | 52 52 52 52 52 52 52 | 17.59 18.64 17.15 16.87 23.55 28.88 15.17 | 0.14 0.23 0.18 0.18 0.15 0.15 | 5.01 5.01 4.63 4.86 5.37 5.03 4.41 |
| Average | | | | | 4.90 |
| | | Remote Stati | lons | | |
| HP-19 HP-20 HP-21 HP-23* HP-24* HP-25 HP-26 | Norris Dam Loudoun Dam Douglas Dam Cherokee Dam Watts Bar Dam Great Falls Dam Dale Hollow Dam Berea, Kentucky | 52 51 37 39 28 26 46 52 | 23.53 14.97 15.20 13.45 4.55 2.75 20.75 22.02 | 0.12 0.05 0.04 0.07 0.10 0.12 0.14 0.05 | 4.36 4.17 1.99 2.51 0.71 0.63 4.26 4.88 |
| Average * Station | s in operation only d | uring latter half | of 1959. | | 2.94 |

TABLE IV

GUMMED PAPER FALL-OUT DATA

Particles/sq. ft.

| Station Number | Location | Number of Samples Taken | Maximum | Minimum | Average |
|-------------------|--------------------|----------------------------|---------|---------|---------|
| | | Perimeter Sta | ations | | |
| HP-11 | Kerr Hollow Gate | 52 | 77.00 | 0.00 | 11.96 |
| HP-12 | Midway Gate | 52 | 97.00 | 0.00 | 12.85 |
| HP-13 | Gallaher Gate | 52 | 84.00 | 0.00 | 10.50 |
| HP-14 | White Wing Gate | 52 | 82.00 | 0.00 | 10.13 |
| HP-15 | Blair Gate | 52 | 97.00 | 0.00 | 12.15 |
| HP-16 | Turnpike Gate | 52 | 76.00 | 0.00 | 9.50 |
| HP-17 | Hickory Creek Bend | 52 | 59.00 | 0.00 | 9.50 |
| Average | | | | • | 10.94 |
| | | Remote Stat | cions | | |
| HP-19 | Norris Dam | 52 | 47.00 | 0.00 | 6.23 |
| HP-20 | Loudoun Dam | 31 | 46.00 | 0.00 | 5.27 |
| HP-21 | Douglas Dam | 37 | 14.00 | 0.00 | 0.51 |
| HP-22 | Cherokee Dam | 39 | 11.00 | 0.00 | 0.90 |
| HP-23* | Watts Bar Dam | 28 | 3.00 | 0.00 | 0.41 |
| HP-24* | Great Falls Dam | 26 | 3.00 | 0.00 | 0.19 |
| HP-25 | Dale Hollow Dam | 46 | 59.00 | 0.00 | 4.54 |
| HP-26 | Berea, Kentucky | 52 | 63.00 | 0.00 | 7.19 |
| | | | | | |

TABLE V RADIOACTIVITY IN RAIN WATER Units of 10-7 $\mu e/ee$

| Station Number | Location | Number of Samples Taken | Maximum | Minimum | Average |
|--|---|--|---|--|---|
| | | Perimeter Sta | tions | | |
| HP-11 Hp-12 HP-13 HP-14 HP-15 HP-16 HP-17 | Kerr Hollow Gate Midway Gate Gallaher Gate White Wing Gate Blair Gate Turnpike Gate Hickory Creek Bend | 44 44 43 39 44 43 | 42.59 40.38 38.72 43.47 39.36 54.84 54.18 | 0.11 0.14 0.12 0.09 0.19 0.15 0.10 | 7.22 6.30 6.10 6.53 5.78 8.82 8.14 |
| | | • | | | |
| | | Remote Stati | ons | | |
| HP-19 HP-20 HP-21 HP-22 HP-23* HP-24* HP-25 HP-26 | Norris Dam Loudoun Dam Douglas Dam Cherokee Dam Watts Bar Dam Great Falls Dam Dale Hollow Dam Berea, Kentucky | 45 49 31 33 23 21 41 44 | 89.98 138.47 36.68 32.20 6.89 8.22 41.00 47.28 | 0.13 0.04 0.06 0.13 0.20 0.07 0.21 0.14 | 11.26 14.65 3.86 4.41 1.32 1.41 8.02 10.14 |
| Average | | | | | 6.88 |

TABLE VI

PROBABLE AVERAGE CONCENTRATION OF RADIOACTIVITY IN THE CLINCH RIVER AT MILE 20.8

Units of $10^{-7} \mu c/cc$

| Number of Samples Taken | Maximum | Minimum | Average | $\%$ of $\left(exttt{MPC} ight)_{	exttt{W}}$ |
|----------------------------|---------|---------|---------|---|
| 365 | 36.4 | 0.37 | 3.1 | 25.4 |

TABLE VII

AVERAGE CONCENTRATION OF MAJOR RADIOACTIVE CONSTITUENTS IN THE CLINCH RIVER

1959

| | | | , | Units of 10 ⁻⁸ µc/cc | 10-8 µc |)cc | | Concen. of | $(MPC)^a_{\overline{M}}$ | 9 9 |
|----|-----------------------|--|-----------|---------------------------------|-------------------------------|--|---------|-----------------|--------------------------|--------|
| | Location | Sampling Period | Sr90 | Cel ⁴⁴ | cs137 | Sr90 Cel44 Cs157 RulO5-106 Co60 | 0900 | hc/cc x 10-8 | po/on | MPC |
| | Clinch River | | | | | Andreas de la companya del la companya de la compan | | | | |
| | Mi. 37.5 | 10/1/59 - 1/29/60 | 0.11 | 0.10 | * | * | * | 0.45 | 0.21 | 2.14 |
| | Mi. 20.8 ^b | 12/28/58 - 12/27/59 | 2.00 | 1.5 | 1.9 | 4.7 | 1.8 | 31.0 | 1.22 | 25.4 |
| | Mi. 4.5 | 10/23/58 - 11/3/59 | 1.86 0.54 | 0.54 | 0.53 | 1.14 | 0.23 | 4.9 | 0.22 | 22.3 |
| 14 | | a Weighted average (MPC) $_{ m W}$ calculated for the mixture using (MPC) $_{ m W}$ values for specific radionuclides recommended in the NBS Handbook 69. | ne mixtu | re using | $(\mathrm{MPC})_{\mathrm{W}}$ | values for s | pecific | radionuclides r | ecommend | ed. |

 $^{\mathrm{b}}$ values given for this location are calculated values based on the levels of waste released and the dilution afforded by the river.

^{*} None detected.

TABLE VIII

EXTERNAL GAMMA RADIATION LEVELS

mr/hr

| Dec. Avg. | .106 none .024 | .019 | | .027 | 750. " | ,024 |
|-------------------|----------------|---------------------|---------------------------|---------------|-----------------|---------|
| Nov. | 1 | .013 | ı | • | .019 | |
| Sept. Oct. Nov. | .015 | ,014 | .016 | .022 | .019 | |
| | .020 | .019 | .022 | .025 | .025 | |
| July Aug. | .019 | .015 | .015 | .021 | .018 | |
| | .025 | .022 | .023 | .025 | .036 | |
| June | .028 | .017 | .024 | .034 | .035 | |
| May | .033 | .026 | .026 | .032 | .029 | |
| Mar. Apr. | .027 | .020 | .023 | .030 | .032 | |
| Mar. | .028 | .024 | .025 | .030 | .022 | |
| Feb. | .026 | .021 | .020 | .025 | .028 | |
| Jan. | .022 | .016 | .018 | .025 | .031 | |
| 1 Location | Solway Gate | Y-12 East Portal | Newcomb Road Oak Ridge | Gallaher Gate | White Wing Gate | වි |
| Station Number | ч | CU | 2 | 17 | 5 | Average |

OAK RIDGE GASEOUS DIFFUSION PLANT (K-25)

The results of environmental sampling by the ORGDP during 1959 indicate little, if any, radioactive material contamination of air, soil, or water either inside the plant boundaries or in the plant environs. In all cases, values measured were only small fractions of the recommended maximum permissible concentrations.

With respect to air-borne contamination, monitoring of the general air well within plant boundaries (averaging about 225 eight-hour samples per quarter) revealed no indication of activities approaching the permissible limits (general population) within these boundaries for even short periods. Thus, it appears essentially impossible that any significant air contamination problems can occur outside the ORGDP area.

Plant wastes released into public waterways are monitored at least weekly to insure that the concentration of these materials in the streams leaving the plant boundaries does not exceed the permissible limits given in NBS Handbook No. 69 for drinking water for population in the neighborhood of a controlled area. Monitoring points in Poplar Creek and Clinch River are both upstream and downstream from ORGDP. There were no instances of water release at the plant boundaries above the long-term maximum permissible concentration even for as short a time as the weekly sampling period, and the average activity in Poplar Creek below the plant for the entire year was only 0.03% of the maximum permissible concentration for the discharge of natural uranium; the levels in the Clinch River were much less than this figure.

ENVIRONMENTAL SAMPLING OAK RIDGE GASEOUS DIFFUSION PLANT

1959

| Location of Point | Type of Analysis Made | No. of Samples | Plan | Concentratio | n (µс | Concentration ($\mu c/cc \times 10^{-8}$) t Experience Max. Permissible High Av. (MPC) | Av. Pl. Exp./MPC |
|----------------------------|--------------------------|-------------------|---------|-----------------|-----------|--|------------------|
| Local Streams (Water) | | | ٠ | | | | |
| Poplar Creek | Uranium Concen- | | | | | | |
| Upstream | | 52 | 3.7 | 8.7 | 6.2 | 2000 | 0.51% |
| Downstream | п | 52 | 0.5 | 1.0 | 9.0 | 2000 | 0.03% |
| Clinch River | | | | | | | |
| Upstream | ± | 52 | 0.08 | 0.2 | 0.1 | 2000 | 0.005% |
| Downstream | z | 52 | 0.1 | 0.3 | 0.3 | 2000 | 0.015% |
| | | | | | | | |
| Poplar Creek | Total Beta | | | | | | |
| Upstream | 701 | 52 | 14.0 | 22.0 | 18.0 | 2000 | %6.0 |
| Downstream | = | 52 | 11.0 | 32.0 | 22.0 | 2000 | 1.1% |
| Clinch River | | | | | | | |
| Upstream | Ξ | 52 | 13.0 | 0.96 | 39.0 | 105* | 37.0% |
| Downstream | Ξ | 52 | 10.0 | 136.0 | 50.0 | 105* | 48.0% |
| Normal Sampling Frequency: | quency: Continuous | s sampling; | composi | composited over | one week. | | |

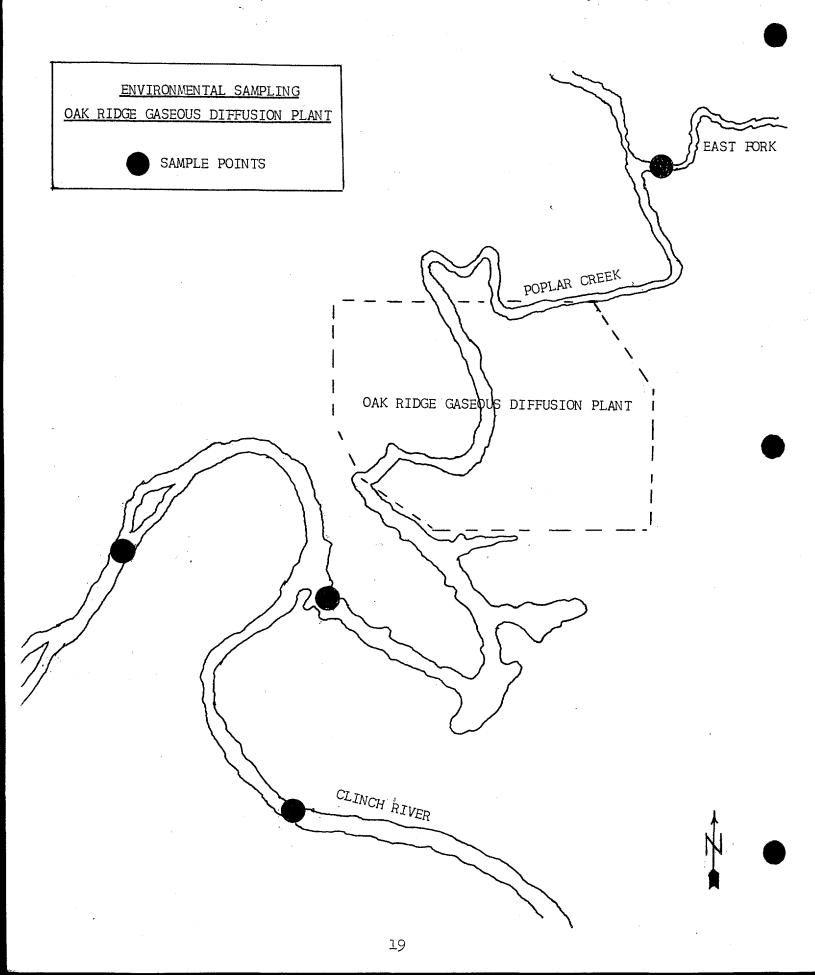
Measured mixture of radionuclides.

ENVIRONMENTAL SAMPLING OAK RIDGE GASEOUS DIFFUSION PLANT

1959

| Location of Point | Type of Analysis Made | No. of Samples | Pl: Low | Concenant Exper High | tration (ience <u>Av.</u> | μc/g x 10-8) Max. Permissible (MPC) |
|---------------------|----------------------------|-------------------|------------|-------------------------|----------------------------------|-------------------------------------|
| Stream Bottom (Mud) | | | | | | |
| Poplar Creek | Uranium Con- centration | | | | | |
| Upstream | Centracton | 4 | 400 | 6900 | 3200 | None Specified |
| Downstream | 11 | 4 | 1300 | 4500 | 2500 | phecilied |
| Clinch River | | | | | | |
| Downstream | n . | 4 | 300 | 1300 | 700 | |
| Poplar Creek | Total Beta Activity | | | | | |
| Upstream | 110017103 | 14 | 7200 | 28,600 | 18,000 | None Specified |
| Downstream | 19 | 14 | 12,900 | 21,200 | 18,500 | opecii ieu |
| Clinch River | | | | | | |
| Downstream | 11 | 4 | 15,800 | 79,200 | 45,500 | |

Normal Sampling Frequency: Grab sample, once each quarter at each location.



Y-12 PLANT

The Y-12 Plant does not monitor the air and water outside the plant area. However, in-plant monitoring indicates that the plant levels are well below the limits for environmental levels.

May 28, 1960

ENVIRONMENTAL LEVELS OF RADIOACTIVITY FOR THE OAK RIDGE AREA

Report for 1959

Data Compiled by: H. H. Abee

APPROVAL FOR RELEASE

Document: # Unnumbered ; Date 5/28/60 ;
Title/Subject ENVIRONMENTAL LEVELS OF RADIOACTIVITY

FOR THE OAK RIDGE AREA

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Date

#506

Introduction

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Solid wastes are buried in a Conasauga shale formation. This shale has a marked ability to fix radioactive materials by an ion exchange mechanism.

Liquid wastes which contain long-lived fission products are confined in storage tanks or are released to earthen pits located in the Conasauga shale formation. Low level liquid wastes are discharged, after preliminary treatment, to the surface streams.

Air that may become contaminated by radioactive materials is exhausted to the atmosphere from several tall stacks after treatment by means of filters, scrubbers, and/or precipitators.

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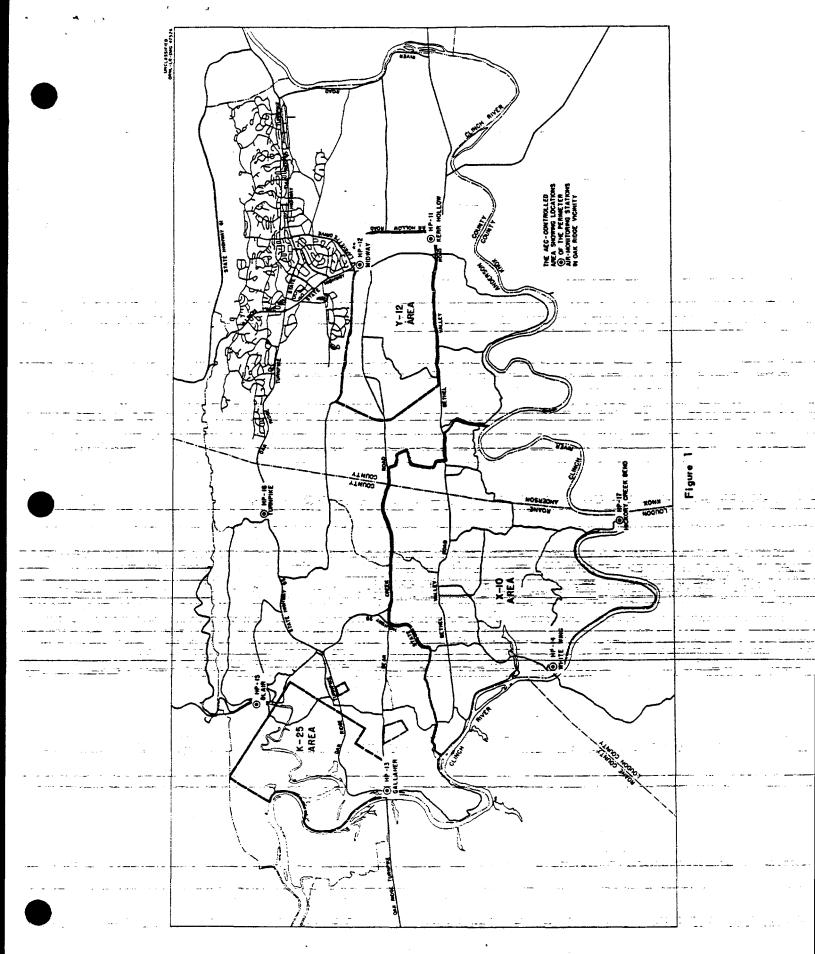
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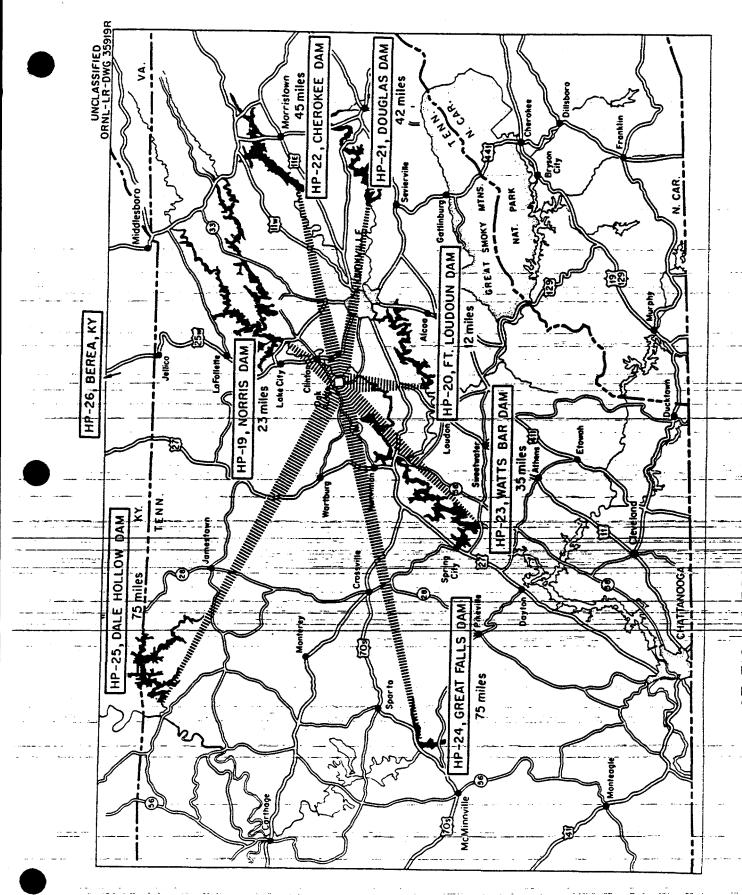
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Water Monitoring

National Laboratory are discharged, after some preliminary treatment, into the Tennessee River system by way of White Oak Creek and the Clinch River. Liquid wastes originating at the Oak Ridge Gaseous Diffusion Plant and the Y-12 Plant are discharged to Poplar Creek and thence to the Clinch River. Releases are controlled so that resulting average concentrations in the Clinch River comply with the maximum permissible levels for population in the neighborhood of a controlled area as recommended by the National Committee on Radiation Protection (NCRP).

The concentration of radioactivity leaving White Oak Creek is measured and concentration values for the Clinch River are calculated on the basis of the dilution provided by the river.





AIR MONITORING SYSTEM REMOTE TES 2 STATION

Δ

Radioactive liquid wastes are sampled at a number of locations as shown in Figs. 3 and 4. Samples are taken in Poplar Creek and White Oak Creek prior to entry of the wastes into the public waterway and at a number of locations in the Clinch River, beginning at a point above the entry of wastes into the river and ending at Center's Ferry near Kingston, Tennessee. Stream gauging operations are carried on continuously by the United States Geological Survey to obtain dilution factors for calculating the probable concentrations of wastes in the river.

The fraction of the total beta activity comprised by each isotope is determined from analysis of long-lived radionuclides contained in the effluent and a weighted average maximum permissible concentration for water, $(MPC)_{\rm W}$, for the mixture of radionuclides is calculated on the basis of the isotopic distribution using the MPC values of each isotope as recommended by the NCRP. The average concentrations of radioactivity in the Clinch River are compared to the calculated $(MPC)_{\rm W}$ value.

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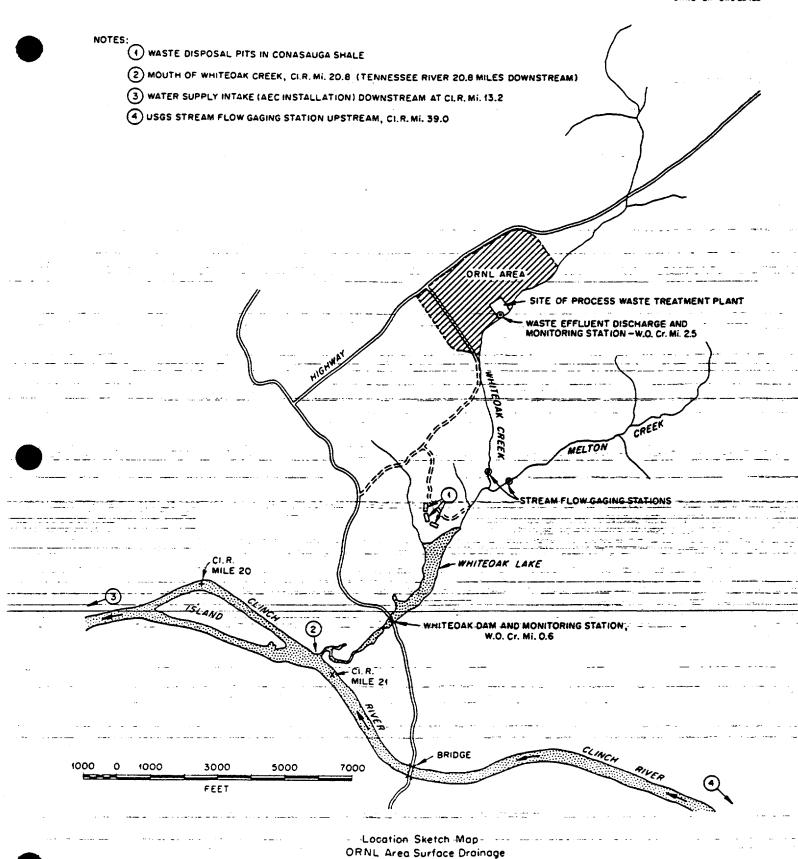
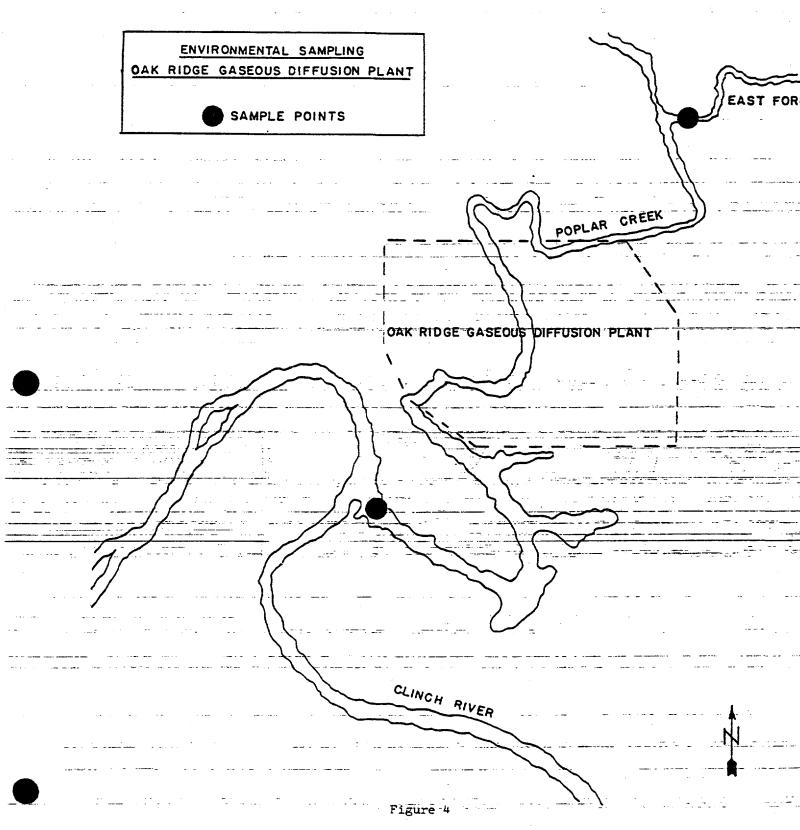


Figure 3



average. Specific analysis for fission products and decay studies indicated that the high levels experienced during the first part of the year were due to the type of fall-out from world-wide weapons testing. The low values for remote stations 23 and 24 resulted from the fact that these stations were in operation only during the latter half of 1959 and do not reflect the higher fall-out levels experienced during the first half of the year.

Fall-out data and rain water data followed the same trend shown by the continuous air monitoring data.

The probable average concentrations of radioactivity in the Clinch River at Mile 20.8, the point of entry of the wastes, and at Mile 4.5, near Kingston, Tennessee, were 3.1 x 10-7 μ c/cc and 4.9 x 10-8 μ c/cc respectively. These values are 25.4% and 22.3% of the weighted average maximum permissible concentration for populations in the neighborhood of a controlled area as recommended by the NCRP. The average concentration of transuranic alpha emitters in the Clinch River at Mile 20.8 was 3 x 10-10 μ c/cc, which is 0.03% of the weighted average (MPC)w value. The average activity in Poplar Creek below the ORGDP for the entire year was only 0.03% of the maximum permissible concentration for natural uranium.

The concentration of radioactivity in the sediment of the Clinch River drops off materially after the first 20 miles downstream from the entry of White Oak Creek and approaches background levels 200 miles downstream. The average radiation level for the cross section where the highest levels were encountered was approximately 19 times the measured background levels or 0.12 mr/hr. This point is located 4.5 miles below the outfall of White Oak Creek. At 100 miles downstream the average level was approximately twice background.

External gamma radiation levels in the Oak Ridge area averaged 0.024 mr/hr. This level does not differ significantly from the average of the levels measured throughout the United States by the U.S. Public Health Service Radiation Surveillance Network.

TABLE I

CONTINUOUS AIR MONITORING FILTER DATA Units of $10^{-13} \, \mu \text{c/cc}$

| Station Number | Location | Number of | Maximum | Minimm | Average | 46 (ME |
|---|--|--|--|--|--|-------------------------------------|
| | | Perimeter St | ations | | | |
| HP-11 | Kerr Hollow Gate | 52 | 47.52 | 0.49 | 15.77 | 1 |
| HP-12 | Midway Gate | 49 | 81.31 | 0.08 | 16.29 | |
| HP-13 | Gallaher Gate | 5 <u>2</u> | 58.52 | 0.54 | 16.63 | |
| HP-14 | White Wing Gate | 52 | 42.48 | 0.49 | 11.30 | |
| HP-15 | Blair Gate | 52 | 61.06 | 0.45 | 19.97 | |
| HP-16 | Turnpike Gate | 52 | 51.6 1 | 0.28 | 13.48 | |
| HP-17 | Hickory Creek Bend | 52 | 60.27 | -0.17 | 16.86 | |
| | | a a man de | | | i i i i i i i i i i i i i i i i i i i | |
| Average | The same of the sa | | | | - 15.76- | |
| | | | | | | |
| | | | | | | |
| | | Demoto Ctot | | | and the second s | |
| | | Remote Stat | ions | | | |
| HP-19 | Norris Dam | Marine and the second s | 10ns 86.20 | 0.57 | 23.23 | |
| - | Norris Dam Loudoun Dam | Remote Stat | 86.20 | 0.57 0.65 | 23.23 | |
| HP-20 | | 52 | 86.20 90.49 | 0.65 | 22.11 | : |
| HP-20 HP-21 HP-22 | Loudoun Dam | 52 52 | 86.20 90.49 58.17 | | | · · · · · · · · · · · · · · · · · · |
| HP-20 HP-21 HP-22 | Loudoun Dam Douglas Dam | 52 52 37 | 86.20 90.49 | 0.65 0.68 | 22.11 10.91 | |
| HP-19 HP-20 HP-21 HP-22 HP-23** | Loudoun Dam Douglas Dam Cherokee Dam | 52 52 37 39 | 86.20 90.49 58.17 100.52 | 0.65 0.68 0.52 | 22.11 10.91 16.01 5.13 | 2 2 3 |
| HP-20 HP-21 HP-22 HP-23** HP-24** | Loudoun Dam Douglas Dam Cherokee Dam Watts Bar Dam | 52 52 37 39 | 86.20 90.49 58.17 100.52 35.14 | 0.65 0.68 0.52 0.49 | 22.11 10.91 16.01 | |
| HP-20 HP-21 HP-22 HP-23** HP-24** | Loudoun Dam Douglas Dam Cherokee Dam Watts Bar Dam Great Falls Dam | 52 52 37 39 29 26 | 86.20 90.49 58.17 100.52 35.14 10.58 | 0.65 0.68 0.52 0.49 0.24 | 22.11 -10.91 -16.01 -5.13 2.53 | (|
| HP-20 HP-21 HP-22 HP-23** HP-24** | Loudoun Dam Douglas Dam Cherokee Dam Watts Bar Dam Great Falls Dam Dale Hollow Dam | 52 52 37 39 29 26 46 | 86.20 90.49 58.17 100.52 35.14 10.58 78.91 | 0.65 0.68 0.52 0.49 0.24 0.76 | 22.11 -10.91 -16.01 -5.13 -2.53 -18.04 | (|

^{* (}MPC)a is taken to be 10^{-10} µc/cc as recommended in NBS Handbook 69, Table 4, p. 94. ** Stations in operation only during latter half of 1959.

TABLE II

CONTINUOUS AIR MONITORING FILTER DATA Particles/1000 cu. ft. of Air Sampled

| Number | Location | Samples Taken | Maximum | Minimum | Aver |
|---|--|--|--|--------------------------------------|--|
| | | Perimeter Stati | ons | | |
| HP-11 | Kerr Hollow Gate | 52 | 6.27 | 0.00 | 1.2 |
| HP-12 | Midway Gate | 49 | 6.81 | 0:00 | 1.2 |
| HP-13 | Gallaher Gate - | 52 | 5.08 | 0.00 | 0.9 |
| HP-14 | White Wing Gate | 52 | 5.91 | 0:00 | 8 |
| HP-15 | Blair Gate | 52 | 10 . 29 | 0:00 | 1.5 |
| HP-16 | Turnpike Gate | 52 | 5.39 | 0.00 | 0.8 |
| HP-17 | Hickory Creek Bend | 52 | 7.22 | 0.00 | 1.0 |
| | | | · | | |
| Average | | | A SA COMPANY OF THE SAME OF TH | | 1.0 |
| Average | | | | | 1.0 |
| Average | | Remote Station | S | | 1.0 |
| Average HP-19 | Norris Dam | Remote Station | s 7.98 | 0.00 | 1.6 |
| | Norris Dam Loudoun Dam | 52 52 | 7.98 6.61 | 0.00 | 1.6 |
| HP-19 | | | 7.98 | 0.00 | 1.6 1.4 0.2 |
| HP-19 HP-20 | Loudoun Dam | 52 52 37 39 | 7.98 6.61 2.83 7.26 | 0.00 0.00 0.00 | 1.6 1.4 0.2 0.5 |
| HP-19 HP-20 HP-21 HP-22 HP-23* | Loudoun Dam Douglas Dam Cherokee Dam Watts Bar Dam | 52 52 37 39 29 | 7.98 6.61 2.83 7.26 0.40 | 0.00 0.00 0.00 | 1.6 1.4 0.2 0.5 |
| HP-19 HP-20 HP-21 HP-22 HP-23* HP-24* | Loudoun Dam Douglas Dam Cherokee Dam Watts Bar Dam Great Falls Dam | 52 52 37 39 29 26 | 7.98 6.61 2.83 7.26 0.40 0.14 | 0.00 0.00 0.00 0.00 | 1.6 1.4 0.2 0.5 0.0 |
| HP-19 HP-20 HP-21 HP-22 HP-23* HP-24* HP-25 | Loudoun Dam Douglas Dam Cherokee Dam Watts Bar Dam Great Falls Dam Dale Hollow Dam | 52 52 37 39 29 26 46 | 7.98 6.61 2.83 7.26 0.40 0.14 | 0.00 0.00 0.00 0.00 0.00 | 1.6 1.4 0.2 0.5 0.0 0.0 |
| HP-19 HP-20 HP-21 HP-22 HP-23* HP-24* | Loudoun Dam Douglas Dam Cherokee Dam Watts Bar Dam Great Falls Dam | 52 52 37 39 29 26 | 7.98 6.61 2.83 7.26 0.40 0.14 | 0.00 0.00 0.00 0.00 | 1.6 1.4 0.2 0.5 0.0 |

TABLE III

GUMMED PAPER FALL-OUT DATA

Units of $10^{-4} \mu c/sq$. ft.

<u> 1959</u>

| Station Number | Location | Number of Samples Taken | Maximum | Minimum | Avera |
|---|--|----------------------------------|--|--|--|
| | | - Perimeter Stat | ions | | |
| -HP-11 | Kerr Hollow Gate | <u>52</u> | 17:59 | -0:14 | 5:01 |
| HP-12 | Midway Gate | 52 | 18.64 | 0.23 | 5.01 |
| HP-13 | Gallaher Gate | 52 | 17.15 | 0.18 | 4.63 |
| HP-14 | White Wing Gate | 52 | 16.87 | 0.18 | 4.86 |
| HP-15 | Blair Gate | 52 | 23.55 | 0.15 | 5.37 |
| HP-16 | Turnpike Gate | 52 | 28.88 | 0.15 | 5.03 |
| HP-17 | Hickory Creek Bend | 52 | 15.17 | 0.14 | |
| | | | | | |
| | | | | | |
| Average | | | | | 4.90 |
| Average | | Remote Station | | | 4.90 |
| 200 200 200 200 200 200 200 200 200 200 | Normis Dam | *** | | 0.10 | |
| HP-19 | Norris Dam | 52 | 23.53 | 0:12 | 4.36 |
| HP-19 HP-20 | Loudoun Dam | 52 51 | 23.53 14.97 | 0:05 | 4.36 4.17 |
| HP-19 HP-20 HP-21 | Loudoun Dam Douglas Dam | 52 51 .37 | 23.53 14.97 15.20 | 0.05 0.04 | 4.36 4.17 1.99 |
| HP-19 HP-20 HP-21 HP-22 | Loudoun Dam Douglas Dem Cherokee Dam | 52 51 37 39 | 23.53 14.97 15.20 13.45 | 0.05 0.04 0.07 | 4.36 4.17 1.99 2.51 |
| HP-19 HP-20 HP-21 | Loudoun Dam Douglas Dam Cherokee Dam Watts Bar Dam | 52 51 .37 .39 28 | 23.53 14.97 15.20 13.45 4.55 | 0.05 0.04 0.07 0.10 | 4.36 4.17 1.99 2.51 0.71 |
| HP-19 HP-20 HP-21 HP-23* HP-24* | Loudoun Dam Douglas Dam Cherokee Dam Watts Bar Dam Great Falls Dam | 52 51 37 39 28 26 | 23.53 14.97 15.20 13.45 4.55 2.75 | 0.05 0.04 0.07 0.10 0.12 | 4.36 4.17 1.99 2.51 0.71 0.63 |
| HP-19 HP-20 HP-21 HP-22 HP-23* HP-24* HP-25 | Loudoun Dam Douglas Dam Cherokee Dam Watts Bar Dam Great Falls Dam Dale Hollow Dam | 52 51 37 39 28 26 | 23.53 14.97 15.20 13.45 4.55 2.75 | 0.05 0.04 0.07 0.10 0.12 0.14 | 4.36 4.17 1.99 2.51 0.71 0.63 4.26 |
| HP-19 HP-20 HP-21 HP-23* HP-24* | Loudoun Dam Douglas Dam Cherokee Dam Watts Bar Dam Great Falls Dam | 52 51 37 39 28 26 | 23.53 14.97 15.20 13.45 4.55 2.75 | 0.05 0.04 0.07 0.10 0.12 | 4.36 4.17 1.99 2.51 0.71 0.63 |

TABLE IV

GUMMED PAPER FALL-OUT DATA

Particles/sq. ft.

| Station Number | Location | Number of Samples Taken | Maximum | Minimum | Avera |
|--|--|----------------------------------|--|------------------------------|--|
| | | Perimeter Stati | ons - | | |
| HP-11 | Kerr Hollow Gate | 52 | 77:00 | 0.00 | 11.9 |
| HP-12 | Midway Gate | 52 | 97.00 | 0.00 | 12.8 |
| HP-13 | Gallaher Gate | 52 | 84.00 | 0.00 | 10.5 |
| HP-14 | White Wing Gate | 52 | 82.00 | 0.00 | 10.1 |
| HP-15 | Blair Gate | 52 | 97.00 | 0.00 | 12.1 |
| HP-16 | Turnpike Gate | 52 | 76:00 | 0:00 | 9.5 |
| HP-17 | Hickory Creek-Bend | 52 | 59.00 | 0.00 | 9.5 |
| | | | | | |
| Average | | | | | 10.9 |
| Average | | Remote Station | | | 10.9 |
| Average HP-19 | Norris Dam | | 5 -47.00 | 0:00 | |
| | Norris Dam Loudoun Dam | 52 | December 12 Contraction | 0.00 | 6.23 |
| HP-19 | | | 47:00 | | |
| HP-19 HP-20 | Loudoun Dam | 52 31 | 47.00 46.00 | 0.00 | 6.23 5.27 0.51 |
| HP-19 HP-20 HP-21 | Loudoun Dam Douglas Dam | 52 31 | 47.00 46.00 14.00 | 0.00 | |
| HP-19 HP-20 HP-21 HP-22 | Loudoun Dam Douglas Dam Cherokee Dam | 52 31 37 39 | 47.00 46.00 14.00 11.00 | 0.00 0.00 0.00 | 6.23 5.27 0.51 -0.90 |
| HP-19 HP-20 HP-21 HP-22 HP-23* | Loudoun Dam Douglas Dam Cherokee Dam Watts Bar Dam | 52 31 37 39 28 | 47.00 46.00 14.00 11.00 3.00 | 0.00 0.00 0.00 0.00 | 6.23 5.27 0.51 -0.90 0.41 -0.19 |
| HP-19 HP-20 HP-21 HP-22 HP-23* HP-24* | Loudoun Dam Douglas Dam Cherokee Dam Watts Bar Dam Great Falls Dam | 52 31 37 39 28 26 | 47.00 46.00 14.00 11.00 3.00 | 0.00 0.00 0.00 0.00 | 6.23 5.27 0.51 -0.90 0.41 |

TABLE V

RADIOACTIVITY IN RAIN WATER Units of 10-7 µc/cc

| Station Number | Location | Number of Samples Taken | Maximum | Minimum | Aver |
|-------------------|--------------------|----------------------------|---------|---------|------|
| | | Perimeter Stati | ons | | |
| HP-11 | Kerr Hollow Gate | भेग | 42.59 | 0.11 | 7.2 |
| HP-12 | Midway Gate | 1114 | 40.38 | 0.14 | 6.30 |
| HP-13 | Gallaher Gate | . — | 38.72 | 0.12 | 6.10 |
| HP-14 | White Wing Gate | 43 | 43.47 | 0.09 | 6.5 |
| HP-15 | Blair Gate | 39 | 39.36 | 0.19 | 5.78 |
| HP-16 | Turnpike Gate | 44 | 54.84 | 0.15 | 8.82 |
| HP-17 | Hickory Creek Bend | 43 | 54.18 | -0.10 | 8.1 |
| Average | | | | * | 6.9 |
| | | - Remote Station | S | | |
| HP-19 | Norris Dam | 45 | 89.98 | 0.13 | 11.2 |
| HP-20 | Loudoun Dam | | 138.47 | 0.04 | 14.6 |
| HP-21 | Douglas Dam | | 36.68 | 0.06 | 3.8 |
| HP-22 | Cherokee Dam | 33 | 32.20 | 0.13 | 4.4 |
| HP-23* | Watts Bar Dam | 23 | 6.89 | 0.20 | 1.3 |
| HP-24* | Great Falls Dam | 21 | 8.22 | 0.07 | 1.4 |
| HP-25 | Dale Hollow Dam | 41 | 41.00 | 0.21 | 8.0 |
| | Berea, Kentucky | 44 | 47.28 | 0.14 | 10.1 |
| HP-26 | berea, nemoticity | r r | . 1 | ••• | |

TABLE VI

PROBABLE AVERAGE CONCENTRATION OF RADIOACTIVITY IN THE CLINCH RIVER AT MILE 20.8

Units of 10⁻⁷ µc/cc

<u> 1959</u>

Number of
Samples Taken Maximum Minimum Average % of (MPC)

365 36.4 0.37 3.1 25.4

| 1 | ۲ | ٠ |
|---|---|---|
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| • | 9 | ς |
| Į | 5 | 4 |

| | (MPC) ⁸ 10-6 μc/cc |
|--|--|
| | Probable Avg. Concen. of Radioactivity µc/cc x 10-8 |
| ONSITUENTS | 0900 |
| -0 | uc/cc Ru103-106 |
| MAJOR RADIOAC CLINCH RIVER 1959 | Juits of 10-8 µc/cc |
| OF HE | 1ts 144 |
| ONCENTRATION OF MAJOR RADIOACTIVE IN THE CLINCH RIVER 1952 | Sr ⁹⁰ Ce |
| AVERAGE CON | Sampling Period |
| | Semp |
| | ation |

| Sampling Period Sr 90 | Ce ¹⁴⁴ Cs ¹³⁷ Ru ^{1C} | Ru 103-106 | 99 | Radioactivity $\mu c/cc \times 10^{-8}$ | 10-6 µc/cc | % of MPC |
|--|--|---------------|-------------------|---|---------------|-------------|
| | | | | | | |
| CLINGN KIVer | | - | | | | |
| M1. 37.5 10/1/59 - 1/29/60 0.11 10 | * * | _ * | · -* . | 0.45 | ر در | 9 |
| M1. 20.8 ^b 12/28/58 - 12/27/59 2.00 1 | .5 1.9 | 7.4: | α | , , | j 6 | #T # 10 |
| M1. 4.5 10/23/58 - 11/3/59 1.86 0 | .54 0.53 | - | 6 | 2 0 | יים די על | 4,7,4 |

values based on the levels of waste released and the dilution b Values given for this location are calculated afforded by the river.

^{*} None detected

| | | Ave. | 420° | .019 | .021 | .027 | .027 | , 024 | l | , |
|--|---------------------------------------|----------|----------------|---------------------|---------------------------|---------------|-----------------|-------|---|---------------------------------------|
| | | Dec. | d | | = | = | = | · | | |
| - | | - | | | | | | | | |
| | | Nov. | 910. | .013 | t | t | .019 | | | |
| | | Oct. | .015 | 410. | •016 | .022 | .019 | | | |
| | | Sept. | 020 | .019 | 085 | - 025 | • 025 | | | |
| | | Aug. | .019 | .015 | .015 | -0S | .018 | | | |
| TEVELS | | July | .025 | . d22 | 083 | .025 | -036 | | , | |
| en e | | June | .028 | .017 | #Z05 | •034 | •03\$ | | - | Samilar ya hara |
| TABLE VIII TAMA RADIATION | . 0/1 | Мау | .033 | | .026 | .032 | .029 | | | |
| GAM TA | | Apr | .027 | 020. | 8 | - 93 | e - | | | |
| EXTERN | | Mar. | .028 | 8 | .025 | •030 | 82 | | | |
| | | Feb. | 920. | .021 | .020 | .025 | 88 | | 2 | · · · · · · · · · · · · · · · · · · · |
| | 4-7 | Jan. | . 022 | .016 | .018 | .025 | .031 | | | 1. <u>-</u> |
| | | Location | Jate | + | Road | . Gate | White Wing Gate | | | |
| | | | Solway Gate | Y-12 East Portal | Newcomb Road Oak Ridge | Gallaher Gate | White Wi | D 00 | i | |
| <u></u> | · · · · · · · · · · · · · · · · · · · | Station | r į | വ | m | | 0 1 | AVELA | | |

| | | | Percent (MPC) _w | 0.31 | 0.03 | , 6.0 | 1.1 | | |
|---------------------------|------|-------------------|----------------------------|-----------------------|----------------------|------------------------|----------------------|----------------------------|--|
| | | | (MPC) _W | 5000 | 5000 | 5000 | 2000 | | |
| POPLAR CREEK | | 위 | un Average | | 9 | 18.0 | 25.0 | week. | |
| TABLE IX RADIOACTIVITY IN | 1959 | | Maximum Minimum | 3.7 | 0.5 | 14.0 | 11.0 | one | |
| T T | | of. | запртев мах | 52" 8.7 | 52 1,0 | 52 22.0 | 52 32.0 | ling; composited over | |
| CONCEIN | | | marysis made | Uranium Concentration | | Total Beta Activity | <u> </u> | cy: Continuous samp | |
| | | Location of Point | | Upstream (East Fork) | Downstream (Outfall) | Upstream (East Fork) | Downstream (Outfall) | Normal Sampling Frequency: | |

TABLE X

RADIOACTIVITY IN THE BOTTOM SEDIMENT OF POPLAR CREEK Units of $10^{-8}~\mu\text{c/g}$

1959

| Location of Point | Type of Analysis Made | No. of Samples | Maximum | Minimum | Average |
|----------------------|----------------------------|----------------|---------|---------|---------|
| Upstream (East Fork) | Uranium Con- centration | 4 | 6900 | 400 | 3200 |
| Downstream (Outfall) | # | 4 | 4500 | 1300 | 2500 |
| Upstream (East Fork) | Total Beta Activity | 4- | 28,600 | 7200 | 18,000 |
| Downstream (Outfall) | <u> </u> | 4 | 21,200 | 12,900 | 18,500 |